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Yuan

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(54) **SUPERCONDUCTING MATRIX FAULT
CURRENT LIMITER WITH
CURRENT-DRIVEN TRIGGER MECHANISM**

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Primary Examiner—Stephen W. Jackson

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(65) **Prior Publication Data**

(57) **ABSTRACT**

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(51) **Int. Cl.**⁷ **H02H 7/00**

A modular and scalable Matrix-type Fault Current Limiter (MFCL) that functions as a "variable impedance" device in an electric power network, using components made of superconducting and non-superconducting electrically conductive materials. An inductor is connected in series with the trigger superconductor in the trigger matrix and physically surrounds the superconductor. The current surge during a fault will generate a trigger magnetic field in the series inductor to cause fast and uniform quenching of the trigger superconductor to significantly reduce burnout risk due to superconductor material non-uniformity.

(52) **U.S. Cl.** **361/19; 361/93.9**

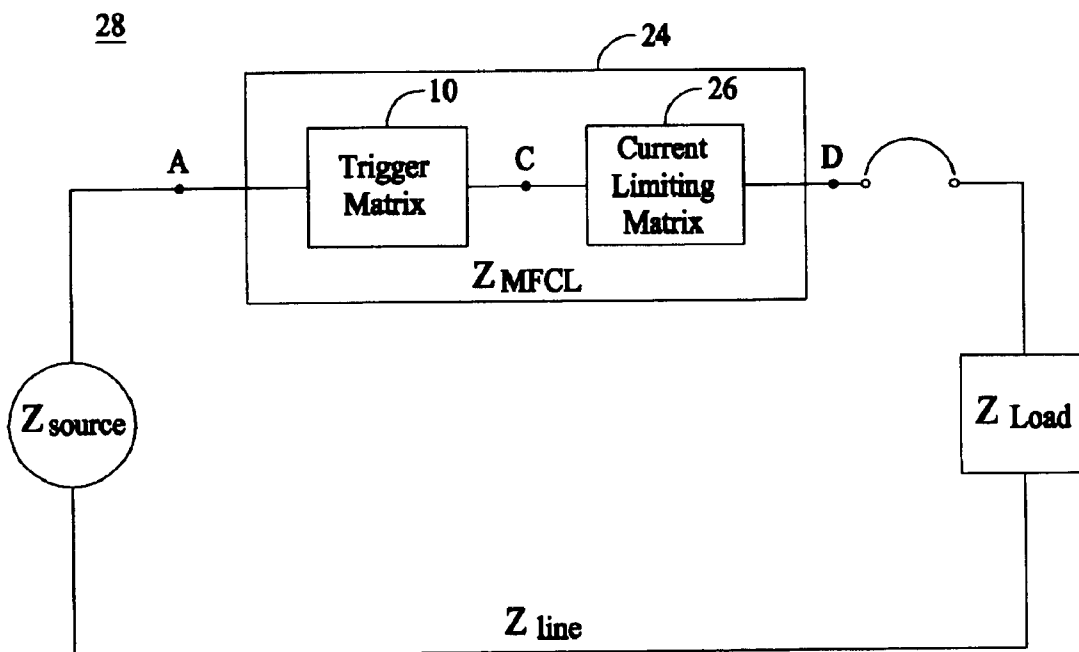
(58) **Field of Search** 361/19, 93.1, 93.9, 361/100, 58

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27 Claims, 7 Drawing Sheets



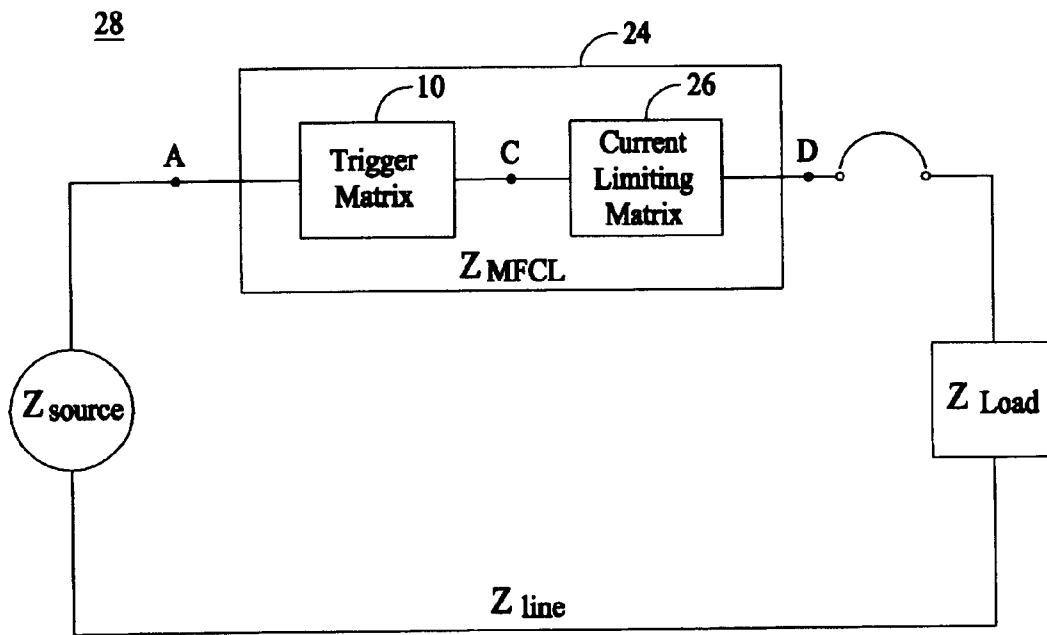


FIG. 1

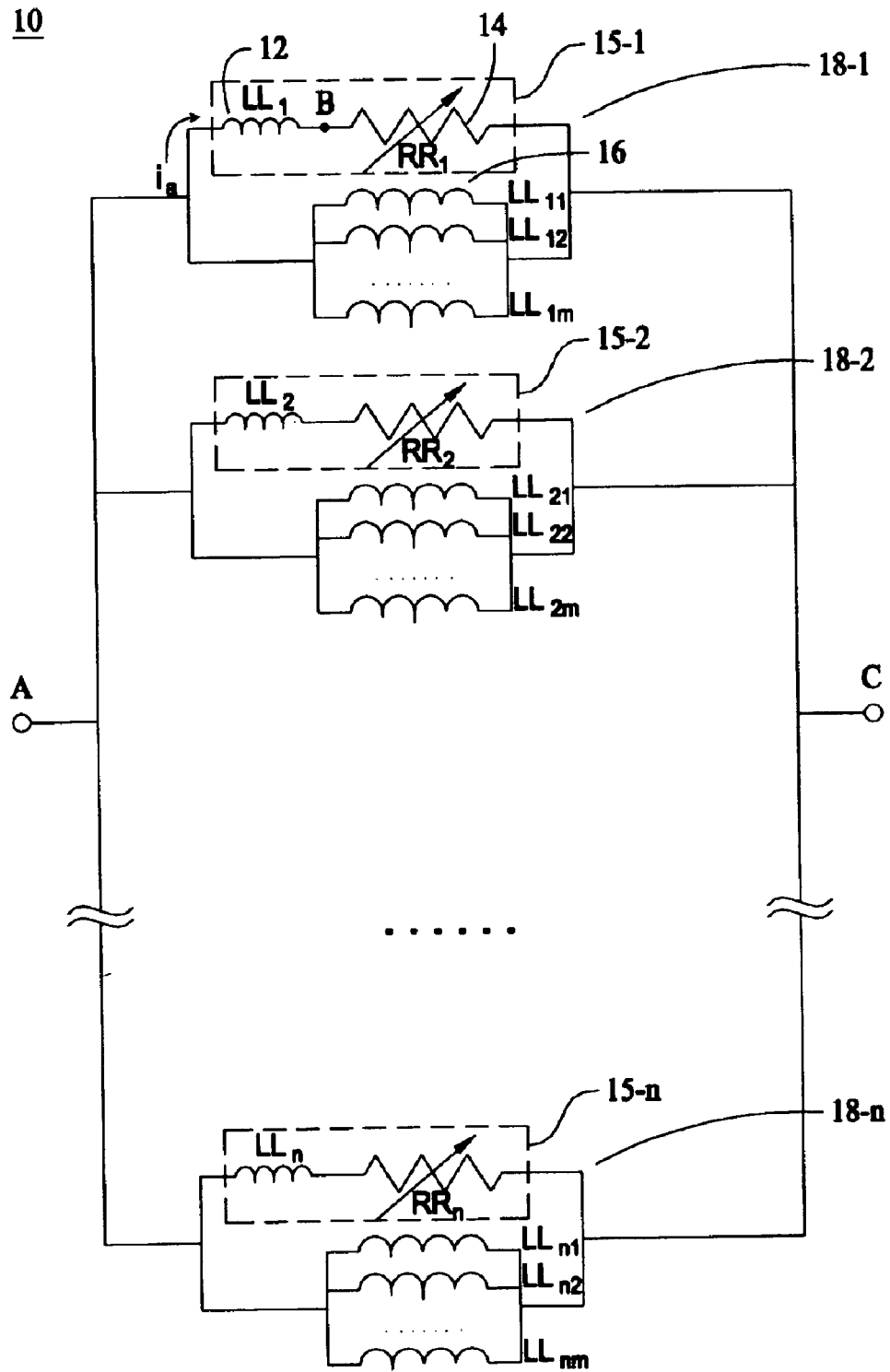


FIG. 2

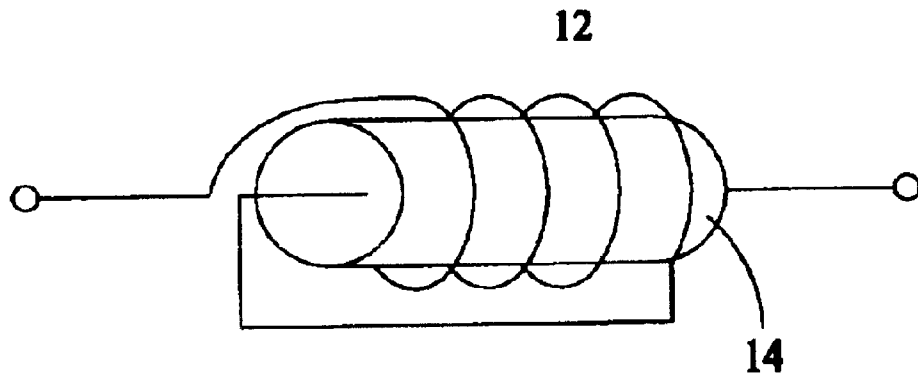


FIG. 3

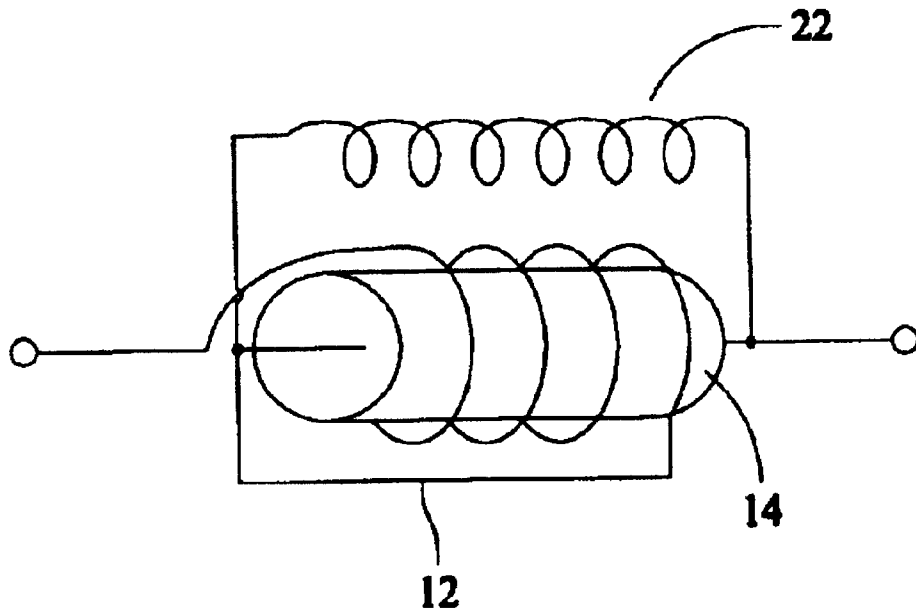


FIG. 5

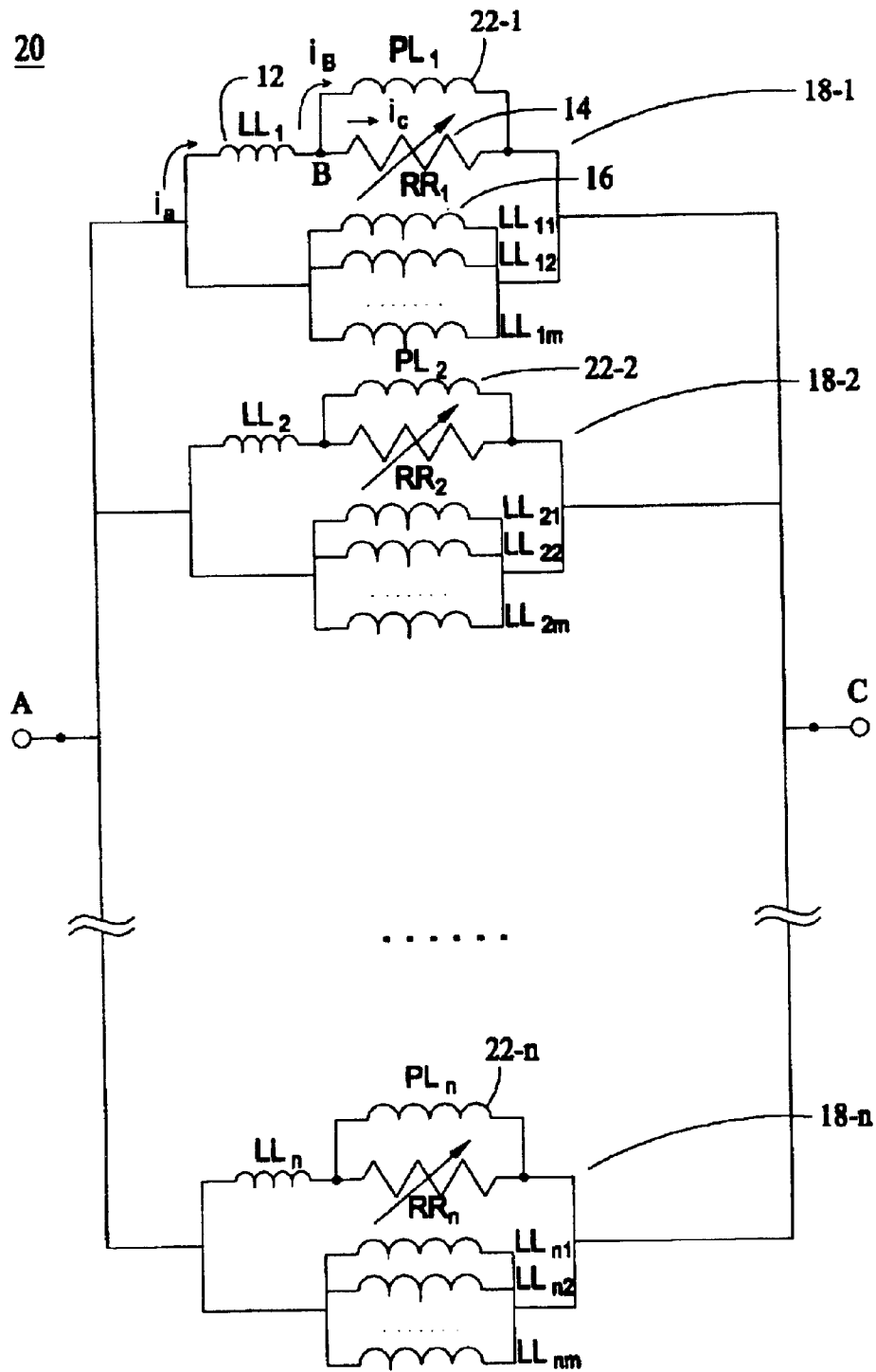


FIG. 4

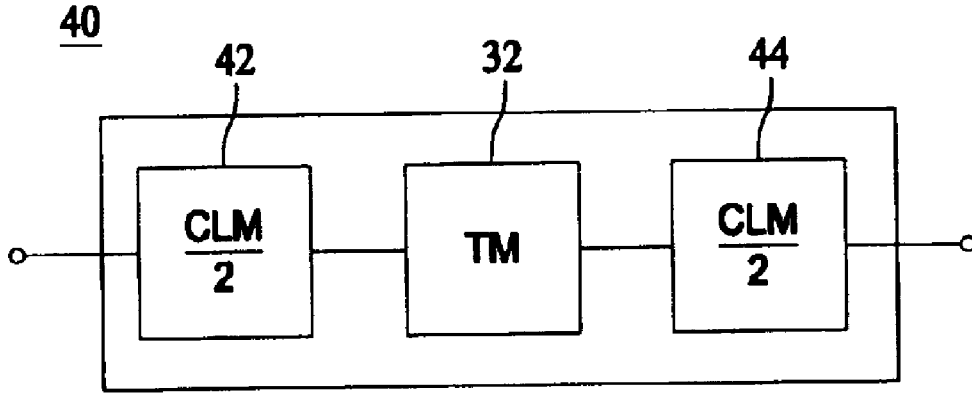


FIG. 6

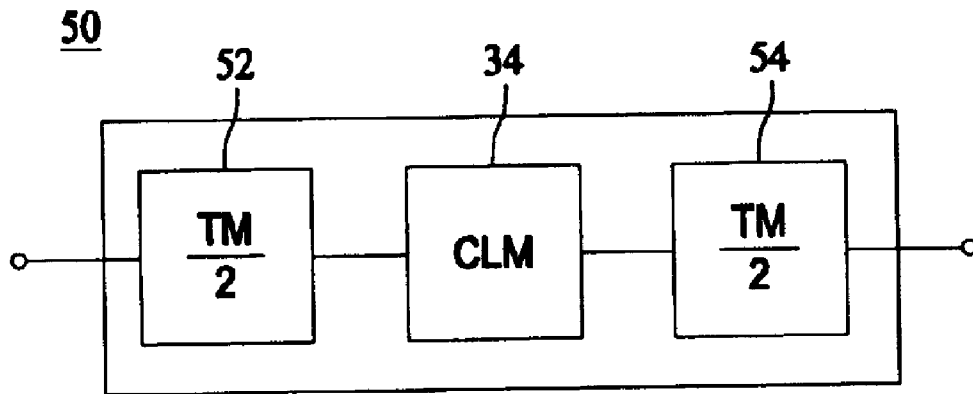


FIG. 7

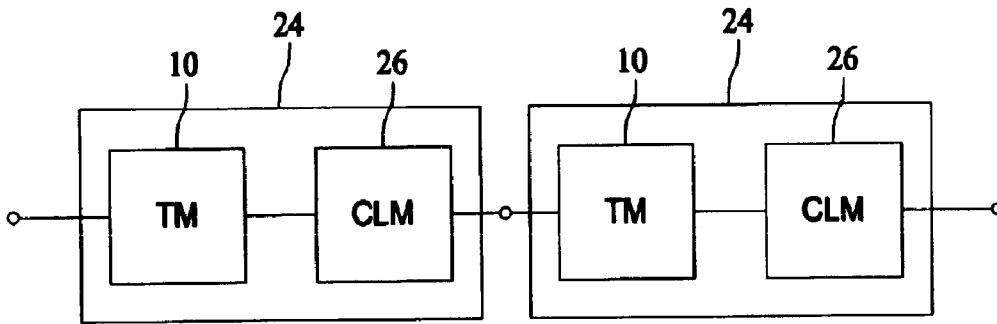


FIG. 8

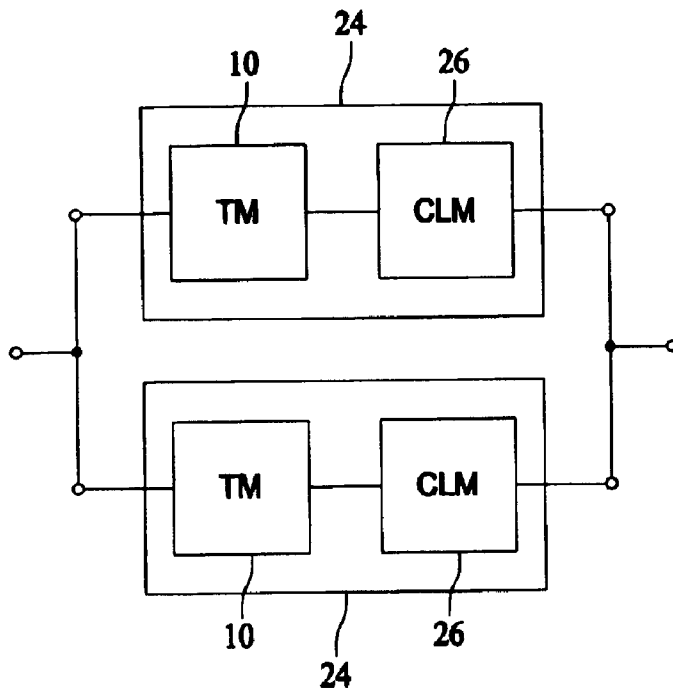


FIG. 9

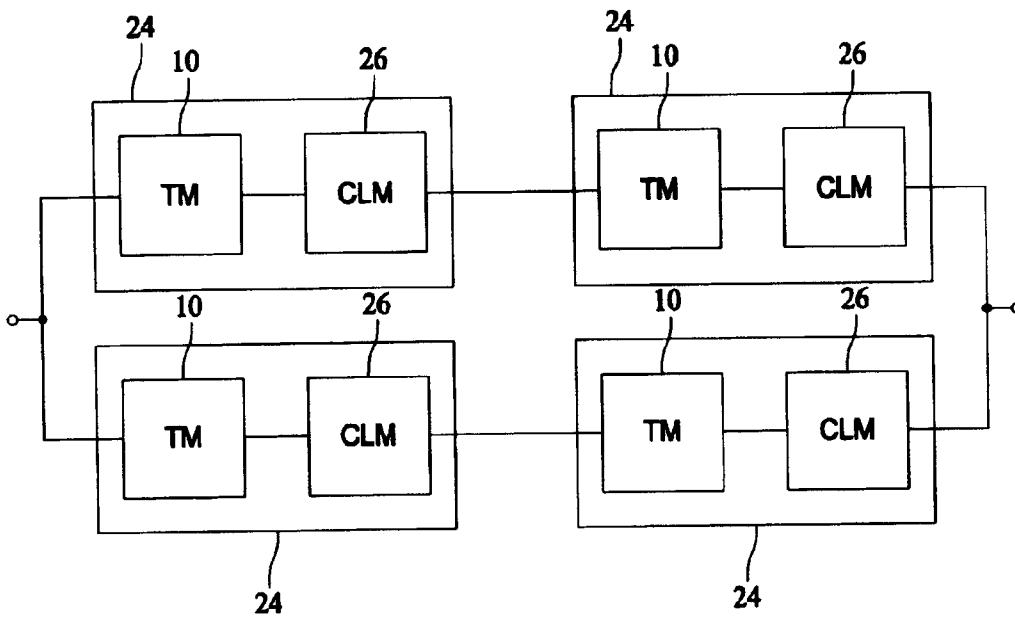


FIG. 10

SUPERCONDUCTING MATRIX FAULT CURRENT LIMITER WITH CURRENT-DRIVEN TRIGGER MECHANISM

BACKGROUND

This invention relates generally to a current limiting device for use in electric power transmission and distribution systems and more particularly to an apparatus for triggering superconductors in a superconducting matrix fault current limiter.

In an existing superconducting matrix fault current limiter (MFCL) configuration (U.S. Publication 2003/0021074 A1, Ser. No. 10/051,671, published Jan. 30, 2003, and assigned to the assignee of the present invention), a trigger matrix is connected in series with a current limiting matrix. The trigger matrix elements are used to provide necessary trigger magnetic fields to assist the transition from a superconducting state to a normal resistive state (the so-called "quenching" of a superconductor), of superconductor elements in the current limiting matrix. Using the first trigger matrix element (310-1 in the application) as an example, the magnetic fields are generated through current sharing between the superconductor trigger element RR_1 and its parallel-connected trigger coils LL_{11} through LL_{m1} . Since LL_{11} through LL_{m1} are physically wound around corresponding individual superconductor element R_{11} through R_{m1} in the current limiting matrix, the magnetic field generated by the current in the trigger coils will cause R_{11} through R_{m1} to quench. In this configuration, the development of current sharing in the trigger matrix is highly dependent on the timely and effective quenching of the superconductor trigger element RR_1 during the initial rise of the fault current. Once the superconductor trigger element RR_1 starts to quench after the fault current surges past its critical current level, a voltage develops across the element itself. This voltage then drives part of the surge current to the trigger coils to create a current-sharing regime.

In the MFCL, a parallel inductor coil LL_1 is physically wound around RR_1 . The current in this coil after the current sharing develops will generate a magnetic field to assist further quenching of RR_1 . However, the initial quench of the RR_1 relies solely on the fault current surging past its critical current level. Therefore, the trigger superconductor elements themselves need to be very reliable in order for the whole MFCL concept to work. These trigger elements should have no or minimal non-uniformity throughout the superconductor volume. The non-uniformity within the superconductor could cause hot spots generated due to uneven quenching and potentially damage the material. It is therefore desirable to have a mechanism, within the MFCL to drive the trigger superconductors to quench uniformly at its initial phase during current limiting, to ensure the successful development of trigger voltage across the trigger matrix and current sharing in the trigger coils.

BRIEF DESCRIPTION

Briefly, in accordance with one embodiment of the present invention, a superconducting matrix fault current limiter (MFCL) is provided which has a trigger matrix section connected in series with a current limiting matrix section, the trigger matrix section has at least one trigger matrix element. Multiple trigger matrix elements can be connected in parallel within a trigger matrix. Each trigger element has at least one non-inductively arranged superconducting component. The superconducting component, herein referred to

as trigger superconductor, is electrically connected in series with an inductor made of electrically conductive material to form a superconducting trigger mechanism. The series inductor is physically disposed around the trigger superconductor in such a way so that the magnetic field generated by the current in the series inductor will be uniformly applied to the trigger superconductor. Under the normal operation condition, the magnetic field generated by the steady current is small enough so that it will not seriously degrade the critical current level of the trigger superconductor. Once there is a fault, the current surge will immediately generate a sufficiently large magnetic field to quench the trigger superconductor. This triggering will happen before or near the start of the quenching process therefore ensuring the trigger superconductor will quench under an uniformed magnetic field with sufficient strength. Such a scheme overcomes non-uniformity existing within the superconductor so that the entire volume of the trigger superconductor will quench simultaneously and uniformly, therefore ensuring the timely development of the current sharing regime. The superconducting trigger mechanism is connected in parallel with a plurality of inductors made of electrically conductive material. These parallel inductors are used to generate adequate magnetic fields once the current sharing develops to trigger superconducting elements in the current limiting matrix.

In an alternative embodiment of the present invention, the superconducting trigger mechanism of the trigger matrix element in a trigger matrix has another component in addition to the trigger superconductor and its series inductor. This additional component is electrically connected in parallel with the trigger superconductor, is made of electrically conductive material and may be an inductor. Such an inductor functions as a shunt of the trigger superconductor. After the trigger superconductor fully quenches, part of its current can be diverted away into the shunt, therefore protecting the superconductor from prolonged heating so that it recovers faster to the superconducting state after current limiting.

The modular nature of the trigger matrix and current limiting matrix arrangement of the MFCL makes it extremely adaptable to high voltage and/or high current operating requirement of the power system to which it connects. For high voltage applications, the one-trigger-matrix-in-series-with-one-current-limiting-matrix becomes one basic building block for an MFCL. Multiple building blocks can be connected in series to form an MFCL that can effectively divide the higher voltage across the terminals into multiple lower-voltage blocks. Such an approach substantially simplifies the dielectric design of an MFCL to meet various high voltage insulation requirements. For high current applications, the basic building blocks are connected in parallel to meet the high current operating requirements. Furthermore, series and parallel connections of these building blocks are utilized to address applications that have both high voltage and high current operating requirements.

DRAWINGS

These and other features, aspects, and advantages of the present invention will become better understood when the following detailed description is read with reference to the accompanying drawings in which like characters represent like parts throughout the drawings, wherein:

FIG. 1 is an illustration of the present invention in an AC circuit that is representative of a single-phase electric power system in its simplest form.

FIG. 2 is a schematic illustration of a trigger matrix of the present invention having an inductor connected in series with a trigger superconductor.

FIG. 3 is an illustration of the physical relationship between the series inductor and the trigger superconductor in a superconducting trigger mechanism within a trigger matrix element of the present invention shown in FIG. 2.

FIG. 4 is a schematic illustration of the component arrangement within a trigger matrix of another embodiment of present invention.

FIG. 5 is an example of the physical relationship between the components of a superconducting trigger mechanism of the embodiment of the present invention shown in FIG. 4.

FIG. 6 is a block diagram of a split current-limiting matrix of the present invention.

FIG. 7 is a block diagram of a split trigger matrix of the present invention.

FIG. 8 is a block diagram of an alternative embodiment of the present invention where the modular trigger and current-limiting matrices of the present invention are arranged in series.

FIG. 9 is a block diagram of an alternative embodiment of the present invention where the modular trigger and current-limiting matrices of the present invention are arranged in parallel.

FIG. 10 is a block diagram of an alternative embodiment of the present invention where the modular trigger and current-limiting matrices of the present invention are arranged in series and then in parallel.

DETAILED DESCRIPTION

FIG. 1 shows an AC circuit 28 that is representative of a single-phase electric power system in its most general form. The AC circuit 28 includes an AC source that is a single-phase power source in a three-phased electricity transmission or distribution network with associated impedance Z_{Source} and overall line impedance Z_{Line} . The AC source supplies a load that has associated impedance Z_{Load} . Electrically connected in series between the AC source and the load is an MFCL 24 device having associated impedance Z_{MFCL} when a fault condition occurs, and a conventional circuit breaker. Absent MFCL 24 in the AC circuit 28, the fault current level when the load is electrically shorted to ground is determined by $i_1 = V_{Source} / (Z_{Source} + Z_{Line})$. However, the inclusion of MFCL 24 in the AC circuit 28 limits the fault current level to a value $i_2 = V_{Source} / (Z_{Source} + Z_{Line} + Z_{MFCL})$. As long as Z_{MFCL} is non-zero when the fault occurs, the i_2 level is lower than i_1 , thus achieving the fault current limiting function. If i_2 is limited to within the designed fault current interrupting capability of the circuit breaker, the circuit breaker will be able to function normally, thereby providing protection to the electric power system and customer equipment.

FIG. 2 shows a schematic diagram of a preferred embodiment of the trigger matrix 10 of the present invention, which includes a plurality of trigger matrix elements 18 (i.e., trigger matrix elements 18-1 through 18-n) electrically connected in parallel between nodes A and D of the MFCL 24 shown in FIG. 1. Each trigger matrix element 18 further includes a superconducting trigger mechanism 15, which comprises of a superconductor component RR 14 and a series inductor LL 12, arranged in parallel with m number of trigger inductors LL 16. For example, the trigger matrix element 18-1 includes a superconducting trigger mechanism 15-1 comprising a superconductor RR₁ arranged in series with a trigger inductor LL₁, connected in parallel with m number of trigger inductors LL₁₁ through LL_{m1} (16-1). Likewise, the trigger matrix element 18-2 includes a super-

conducting trigger mechanism 15-2 comprising a superconductor RR₂ arranged in series with an inductor LL₂, connected in parallel with m number of trigger inductors LL₂₁, through LL_{2m} (16-2). As a last example, the trigger matrix element 18-n includes a superconducting trigger mechanism 15-n including a superconductor RR_n, arranged in series with an inductor LL_n, connected in parallel with m number of trigger inductors LL_{n1} through LL_{nm} (16-n). Superconductor components may be selected from the group including rods, bars, plates, tape strips, tubes and bifilar coils, or other non or low-inductance configurations.

U.S. Patent Publication 2003/0021074 A1, Ser. No. 10/051,671, published on Jan. 30, 2003, assigned to the assignee of the present invention, herein incorporated by reference, describes the interconnection and physical arrangement of the trigger coils in a trigger matrix relative to the components in the current limiting matrix. Because the trigger coils LL 16 of the trigger matrix 10 of the present invention interacts in the same way as described in Publication '074, the details of the interaction of trigger matrix 10 and current limiter matrix 26 will not be described herein.

FIG. 3 shows the physical arrangement of the superconducting trigger mechanism 15. The inductor LL 12 physically surrounds, is wound around and is electrically connected in series with the trigger superconductor RR 14. This physical relationship is repeated for each superconducting trigger mechanism 15 (15-1 through 15-n) in each of the trigger matrix element 18 (18-1 through 18-n) in the trigger matrix 10. The trigger superconductors 14 may assume the forms of a bar, a rod, a tube, a bifilar coil, or any other non- or low-inductive form. The series inductors 12 are made of electrically conductive materials, such as copper, and are selected from the group including helically wound solenoid coils or racetrack or saddle coils. The trigger superconductors 14, along with the rest of the MFCL device, can be housed in a cryostat (not shown). The superconductors are maintained at superconducting state by being cooled below their critical temperature with cooling provided either by coolant within the cryostat or by external cooling mechanisms such as cryocoolers or combination of both.

The operation of the trigger matrix 10 is now described. To achieve high degree of modularity and scalability of the MFCL components, the preferred embodiment assumes all trigger matrix elements 18 (18-1 through 18-n) are identical. This means that within the trigger matrix 10, as illustrated in FIG. 2, all trigger superconductors RR₁ through RR_n are identical, all series inductors LL₁ through LL_n are identical, and all trigger inductors LL₁₁ through LL_{nm} are the same. (Within the current-limiting matrix 26, all superconducting components are assumed to be the same and all non-superconducting components are assumed to be the same.)

The combined critical current level of all the trigger superconductors RR in the trigger matrix 10 under the normal operating condition is designed to be no less than the peak of the nominal AC operating current plus any over-current capacity required by the power system. Each trigger matrix element 18 will see "1/n" of this total current. Within the superconducting trigger mechanism 15 of each trigger matrix element 18, using 15-1 of 18-1 as an example, the series inductor LL₁ is designed to have very low resistance and small inductance so its total impedance is substantially lower than that of the trigger inductors 16 parallel connected to the superconducting trigger mechanism 15. Therefore, of the total current seen by 18-1, only a minimal amount will be current-shared into the parallel trigger inductors 16-1. This minimal amount of current will generate some power losses in the trigger inductors 16. The current will also

generate a magnetic field that will be exerted on the superconducting elements in the current-limiting matrix **26**. However, the level of the magnetic field is very small compare to the critical field level of the superconductors, it will have negligible effect on the critical current level of the superconductors in the current-limiting matrix **26**. The majority of the current seen by **18-1** will then pass the superconducting trigger mechanism **15-1**. The trigger superconductor **14** exhibits no electrical resistance since the current is below its critical current level, and will show no voltage drop across the element since it is also in a non-inductive form. Since the series inductor **12** has very low impedance, so the overall voltage drop across the superconducting trigger mechanism **15-1** is so small as to have negligible impact to the power system to which the MFCL device is connected. The current passing through **18-1** and hence the series inductor **12** will generate a magnetic field in the inductor coil. Because the series inductor is physically disposed around the trigger superconductor **14** as illustrated in FIG. **3**, such a magnetic field will degrade the critical current level of the trigger superconductor **14**. However, as long as the now reduced critical current level of **14** is still higher than the normal operating current seen by **15-1**, the operation of the trigger matrix **10** will not be affected.

When a fault occurs in the power system, the current seen by the superconducting trigger mechanism **15-1** increases to multiples of the normal operating current. Consequently, the magnetic field generated by this surge current in the series inductor **12** increases dramatically and significantly reduces the critical current level of the trigger superconductor **14** it encloses, causing the trigger superconductor **14** to immediately start to quench. Because the magnetic field generated in the series inductor **12** is designed to be uniform, the entire volume of the trigger superconductor **14** is now under a uniformed quench magnetic field, reducing any hot spot burnout risk due to non-uniformity existed within the superconducting material. At the same time when this trigger magnetic field develops, the surged current passing through the trigger superconductor **18** far exceeds the critical current level of the superconductor and drives it to transition from superconducting state to a resistive state. Once the initial quench starts, the subsequent i^2R heating within the trigger superconductor **18** also contributes to the quenching process. Overall, all three factors, namely the current surge, the temperature rise, and the external magnetic field, all work to promote fast and uniform quenching of the trigger superconductor and to prevent its burnout due to material defects.

Once the trigger superconductor RR_1 starts to quench, a substantial voltage drop across the superconducting trigger mechanism **15-1** starts to develop. This voltage will drive to create a meaningful current-sharing regime between the **15-1** and the parallel trigger inductors LL_{11} through LL_{m1} (**16-1**). The shared-current in those trigger inductors **16-1** will then generate sufficient magnetic fields to trigger the superconducting elements in the current-limiting matrix **26**.

The parallelism of the trigger matrix elements **18-1** through **18-n** within the trigger matrix **18** provides built in redundancy in the MFCL **24** design such that a failure of any individual trigger matrix element **18** does not result in the failure of the entire device.

FIG. **4** is an illustration of an alternative embodiment of the present invention. The superconducting trigger mechanism **15** of the trigger matrix element **18** in a trigger matrix **10** has another component **22** in addition to the trigger superconductor **14** and its series inductor **12**. This additional component **22** is electrically connected in parallel with the trigger superconductor **14**, is made of electrically conductive

material and may be an inductor. Such an inductor PL_1 **22** would function as a shunt of the trigger superconductor **14**. After the trigger superconductor **14** fully quenches, part of its current can be diverted away into the shunt PL_1 **22**. This diversion will protect the superconductor **14** from prolonged heating so that it can recover faster to its superconducting state after current limiting.

There are wide-range power system applications for a current limiting device such as an MFCL, especially at the transmission voltage level (loosely defined as voltage at or higher than 100kV line-to-line of a 3-phased system). The modular nature of the trigger matrix and current limiting matrix arrangement of the MFCL makes it well suited for high voltage applications. In addition, the relative placement of trigger matrix (TM) and current limiting matrix (CLM) can be arranged to address the high voltage insulation requirements. FIG. **6** shows one possible arrangement of the trigger matrix **32** and current limiting matrix (**42+44**) that effectively reduce the voltage insulation requirement within the MFCL device **40** by half. FIG. **7** shows another embodiment of the arrangement of trigger matrix (**52+54**) and current limiting matrix **34** that can effectively reduce the voltage insulation requirement within the MFCL **50** by half.

Furthermore, MFCL configurations **24** in FIG. **1**, **40** in FIGS. **6** and **50** in FIG. **7** can be treated as one basic building block for a larger modular MFCL. Multiple such building blocks can be connected in series to form an MFCL that can effectively divide the higher voltage across from terminal to terminal into multiple lower-voltage blocks. Such an approach substantially simplifies the dielectric design of an MFCL to meet various high voltage insulation requirements. FIG. **8** shows one embodiment of using such an approach to form a larger modular MFCL, using trigger matrix **10** and current limiting matrix **26** in an MFCL **24** as an example.

For high current applications, the aforementioned basic building blocks are connected in parallel to meet the high current operating requirements. FIG. **9** shows one embodiment of using such an approach. Again, it uses trigger matrix **10** and current limiting matrix **26** in an MFCL **24** as an example.

For applications that have both high voltage and high current operating requirements, series as well as parallel connections of these basic building blocks may be utilized. FIG. **10** shows one embodiment of using such an approach using trigger matrix **10** and current limiting matrix **26** in an MFCL **24** as an example.

While only certain features of the invention have been illustrated and described herein, many modifications and changes will occur to those skilled in the art. It is, therefore, to be understood that the appended claims are intended to cover all such modifications and changes as fall within the true spirit of the invention.

What is claimed is:

1. A matrix-type superconducting fault current limiter having a current limiting matrix section, said fault current limiter comprising:

a trigger matrix section connected in series with the current limiting matrix section, said trigger matrix section comprising at least one trigger matrix element wherein each respective trigger matrix element is connected in parallel with each other trigger matrix element, each trigger matrix element comprising at least one superconducting trigger mechanism electrically connected in parallel to a plurality of inductors made of electrically conductive material;

wherein within each superconducting trigger mechanism there is at least one series component made of electri-

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cally conductive material that is electrically connected in series with at least one superconducting element, wherein said series component physically surrounds said superconducting element.

2. The fault current limiter as recited in claim 1, wherein each said series component is an inductive coil that is physically wound around the superconducting element of said superconducting trigger mechanism of said trigger matrix element.

3. The fault current limiter as recited in claim 1, wherein each said series component is a resistive foil that is physically surround the superconducting element of said superconducting trigger mechanism of said trigger matrix element.

4. The fault current limiter as recited in claim 1 comprising superconducting components selected from the group including rods, bars, plates, tape strips, tubes, and bifilar coils.

5. The fault current limiter of claim 1, wherein at least two said trigger matrices are arranged in series with at least one said current limiting matrix.

6. The fault current limiter of claim 1, wherein at least one said trigger matrix is arranged in series with at least two said current limiting matrices.

7. The fault current limiter as recited in claim 1, wherein at least two said matrix fault current limiters are arranged in series.

8. The fault current limiter as recited in claim 1, wherein at least two said matrix fault current limiters are arranged in parallel.

9. The fault current limiter as recited in claim 2, wherein the inductive coils are coils made of electrically conductive materials selected from the group including helically-wound solenoid coils, racetrack coils and saddle coils.

10. A matrix-type superconducting fault current limiter having a current limiting matrix section, said fault current limiter comprising:

a trigger matrix section connected in series with the current limiting matrix section, said trigger matrix section comprising at least one trigger matrix element wherein each respective trigger matrix element is connected in parallel with each other trigger matrix element, each trigger matrix element comprising at least one superconducting trigger mechanism electrically connected in parallel to a plurality of inductors made of electrically conductive material;

wherein within each superconducting trigger mechanism is at least one series component made of electrically conductive material that is electrically connected in series with at least one superconducting element, wherein said series component physically surrounds said superconducting element, wherein said superconducting element has at least one parallel connected component made of electrically conductive material.

11. The fault current limiter as recited in claim 10, wherein each of said series components is an inductive coil that is physically wound around the superconducting element of the superconducting trigger mechanism of said trigger matrix element.

12. The fault current limiter as recited in claim 10, wherein each of said series components is a resistive foil that physically surrounds the superconducting element of the superconducting trigger mechanism of said trigger matrix element.

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13. The fault current limiter as recited in claim 10, wherein said parallel component is an inductive coil.

14. The fault current limiter as recited in claim 10, wherein said parallel component is a resistive foil.

15. The fault current limiter as recited in claim 10 comprising superconducting components selected from the group including rods, bars, plates, tape strips, tubes, and bifilar coils.

16. The fault current limiter of claim 10, wherein at least two said trigger matrices are arranged in series with at least one said current limiting matrix.

17. The fault current limiter of claim 10, wherein at least one said trigger matrix is arranged in series with at least two said current limiting matrices.

18. The fault current limiter as recited in claim 10, wherein at least two such matrix fault current limiters are arranged in series.

19. The fault current limiter as recited in claim 10, wherein at least two such matrix fault current limiters are arranged in parallel.

20. The fault current limiter as recited in claim 11, wherein the inductive coils are made of electrically conductive materials and are selected from the group including helically-wound solenoid coils, racetrack coils and saddle coils.

21. A matrix-type superconducting fault current limiter having a current limiting matrix section, said fault current limiter comprising:

a trigger matrix section connected in series with the current limiting matrix section, said trigger matrix section comprising at least one trigger matrix element wherein each respective trigger matrix element is connected in parallel with each other trigger matrix element, each trigger matrix element comprising at least one superconducting trigger mechanism having at least one superconducting element, wherein such mechanism is arranged in parallel to a plurality of inductors made of electrically conductive material.

22. The fault current limiter as recited in claim 21 comprising superconducting components selected from the group including rods, bars, plates, tape strips, tubes, and bifilar coils.

23. The fault current limiter as recited in claim 21, wherein the inductors are coils made of electrically conductive materials selected from the group including helically-wound solenoid coils, racetrack coils and saddle coils.

24. The fault current limiter of claim 21, wherein at least two said trigger matrices are arranged in series with at least one said current limiting matrix.

25. The fault current limiter of claim 21, wherein at least one said trigger matrix is arranged in series with at least two said current limiting matrices.

26. The fault current limiter as recited in claim 21, wherein at least two said matrix fault current limiters are arranged in series.

27. The fault current limiter as recited in claim 21, wherein at least two said matrix fault current limiters are arranged in parallel.

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